Design, Characterisation and Optimisation of a SAW Correlator Driven, Wireless, Passive Microvalve For Biomedical Applications

by

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Abstract

The culmination of rapid advances made in the areas of microelectromechanical systems (MEMS), nonregenerative power sources, nanotechnology, and biomedical engineering have resulted in the expansion of their horizons in modern medicine for the deployment of a wide array of implantable devices. However, the lifetime and remote interrogability of implants, specifically used for drug delivery applications, has been an issue of contention, as their deployment period is limited by the battery life and the device size. Furthermore, not much research effort is directed towards remotely controlled flow manipulation using passive components. These shortcomings are addressed in this thesis by employing surface acoustic wave (SAW) technology to design a novel RF powered, secure coded, active microvalve with fully passive components. By combining the complex signal processing capabilities of the acoustic wave correlator with the electrostatic actuation of the microchannel, the advantages of both the mechanisms are incorporated into a novel microvalve design. Fluid pumping can be achieved at ultrasonic frequencies by electrostatically actuating the edge clamped microchannel, placed in between the compressor interdigital transducer's (IDT's) of two identical SAW correlators. The ability to wirelessly administer doses of drug accurately, for an extended period of time, at an inaccessible target location, through an implanted microvalve has the potential to revolutionise health care for long-term, controlled drug release applications.

Three specific and diverse areas within MEMS, the new device builds on, are investigated by taking a comprehensive design, modelling, optimisation and experimental validation approach for majority of the research endeavors in the thesis. The first area corresponds to SAW technology followed by microfluidics, and body-centric communications; driven by the ultimate goal to demonstrate the operational feasibility of a human implanted, wirelessly controlled microvalve. The proposed specialised design necessitated a thorough understanding of the multiple coupled physics phenomena at the process level, before fabrication, for the critical investigation and refinement of the individual microvalve components. A comprehensive finite element modelling technique, where the complete set of partial differential equations are solved, was used to design these microvalve components with low level of abstraction to enable an automatic inclusion of the majority of the second order effects.

As a starting point for the FEM modelling of SAW devices, an infinite periodic grating was modelled to analyse the freely propagating eigenmodes and eigenvalues with modal analysis; and electrically active waves and electrical admittance with harmonic analysis. A curve fitting technique was employed to extract the COM/P-matrix model parameters from these FEM results. Furthermore, an experimental validation of the parameters extracted using this novel combination of FEM and fitting techniques was carried out by fabricating a number of delaylines and comparing the physical structure response with the formulated P-matrix model. On the other hand, the modelling of a 2 and 3-dimensional, 5×2-bit Barker sequence encoded acoustic wave correlator was demonstrated using FEM. The correlator's response was quantified in terms of harmonic analysis, to obtain the electrical admittance and output voltage profile, and transient analysis, to study the acoustic wave propagating characteristics and correlation pulses. The validation of these simulation results was carried out by fabricating the SAW correlators using optical lithographic techniques. A good agreement between the numerical and experimental results highlighted the feasibility and potential of using FEM for application specific modelling of SAW correlators.

The complexity involved in combining the electroacoustic correlation and electrostatic actuation mechanisms, necessitated a systematic design and optimization of the novel microvalve which is best possible with FEM. In this thesis, the emphasis was on the design and optimisation of a novel microfluidic structure through the deflection analysis, both, to verify the functionality of the concept and to investigate the working range of the structure. Secure interrogability of the microvalve was demonstrated by utilising finite element modelling of the complete structure and the quantitative deduction of the code dependent, harmonic and dynamic transient microchannel actuation. A numerical and experimental analysis of the biotelemetry link for the microvalve was undertaken in the vicinity of numerical and physical human body phantoms, respectively. To accurately account for the path losses and to address the design optimisation, the receiver coil/antenna was solved simultaneously with the transmitter coil/antenna in the presence of a human body simulant using 3-dimensional, high frequency electromagnetic, FEM modelling. The received relative signal strength was numerically and experimentally derived for a miniature ($6 \times 6 \times 0.5$ mm), square spiral antenna/coil when interrogated by a hand-held $8 \times 5 \times 0.2$ cm square spiral antenna/coil in the near field. Finally, the experimental results confirmed well with the FEM analysis predictions and hence ascertained the applicability of the developed system for secure interrogation and remote powering of the newly proposed microvalve.

Statement of Originality

Name: Ajay Chandra Tikka

Program: Doctor of Philosophy (PhD)

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26th October, 2009

Signed

Date

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Abbreviations and Symbols

Abbreviations

AC	Alternating Current
BAW	Bulk Acoustic Wave
BEM	Boundary Element Method
BPSK	Binary Phase Shift Keying
COM	Coupling Of Modes
DC	Direct Current
DIL	Dual In Line
DOF	Degress Of Freedom
EM	Electromagnetic
FDS	Frequency Domain Sampling
FDTD	Finite Difference Time Domain
FEM	Finite Element Method
FM	Frequency Modulation
HFEM	Hybrid Finite Element Method
IDT	Interdigital Transducer
LSAW	Leaky Surface Acoustic Wave
MEMS	Microelectromechanical Systems
MLS	Maximum Length Sequence
MR	Metallization Ratio
PBC	Periodic Boundary Condition
Q-factor	Quality Factor
Q-factor RF	Quality Factor Radio Frequency
RF	Radio Frequency
RF RFID	Radio Frequency Radio Frequency Identification
RF RFID RTO	Radio Frequency Radio Frequency Identification Remote Turn On
RF RFID RTO SAW	Radio Frequency Radio Frequency Identification Remote Turn On Surface Acoustic Wave
RF RFID RTO SAW SDA	Radio Frequency Radio Frequency Identification Remote Turn On Surface Acoustic Wave Spectral Domain Analysis
RF RFID RTO SAW SDA SEM	Radio Frequency Radio Frequency Identification Remote Turn On Surface Acoustic Wave Spectral Domain Analysis Scanning Electron Microscope
RF RFID RTO SAW SDA SEM STW	Radio Frequency Radio Frequency Identification Remote Turn On Surface Acoustic Wave Spectral Domain Analysis Scanning Electron Microscope Surface Transverse Wave

Symbol	Name	Unit
a	displacement vector	m
Α	delayline admittance matrix	mixed
A_0	overlapping area	m ²
В	bandwidth	Hz
B(f)	susceptance	S
С	loaded wavenumber	rad/m
С	stiffness	N/m^2
С	capacitance	F
C_n	normalised capacitance	F
C_p	periodic capacitance	F
D	electrical flux	C/m^2
DR_o	dispersion relation for open circuit grating	-
DR_s	dispersion relation for short circuit grating	-
d	distance	m
E	electric field	V/m
E _c	electromechanical coupling energy	J
E_k	electric field vector	V/m
е	piezoelectric stress constant	C/m^2
F	force	Ν
F_E	electrostatic force	Ν
F^E	nodal electrostatic force	Ν
F_N	noise figure	dB
\mathbf{F}^N	nodal force vector	Ν
\mathbf{F}^{TH}	thermal force vector	Ν
f_c	center frequency	Hz
f_B	bit rate	Hz
f_{M+}	anti-symmetric SAW modal frequency	Hz
f_{M-}	symmetric SAW modal frequency	Hz
G	gain	-
G(x)	Green's function	mixed
G(f)	conductance	S
G(f)	transfer function	mixed
[G]	strain-displacement matrix	mixed
8	spacing between coil turns	m
Н	magnetic field strength	A/m

Symbol	Name	Unit
Ι	current	А
[I]	identity matrix	-
j	unit imaginary number	-
Κ	Boltzmann's constant	-
[K]	structural stiffness matrix	mixed
$[K_d]$	dielectric permittivity matrix	mixed
L	IDT length	m
L	inductance	Н
L _{eff}	effective inductance	Η
l _{avg}	average diameter of the square spiral	m
l _{tot}	total length of the square spiral	m
М	mutual inductance	Н
[M]	mass matrix	mixed
[N]	structural shape function	mixed
$[N_E]$	electrical shape function	mixed
N_B	binary bits	-
п	normalised wavenumber	-
п	number of coil turns	-
Р	power	W
P(f)	P-matrix	mixed
р	period of the grating	m
<i>p</i> _a	radiation pressure	Pa
Q	quality factor	-
9	complex charge of the electrodes	С
q_n	nodal charge density	C/m
R	resistance	Ω
R _s	residual vector of elastostatic field	-
R _e	residual vector of electromechanic field	-
S	strain	-
S ₁₂	insertion loss	dB
S_{P}	power density	W/m^2
SNR	signal-to-noise ratio	-
Т	stress	N/m^2
T_C	temperature	°C
T_B	bit time	sec

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ϕ electrical scalar potentialV σ conductivityS/m² ∇ gradient of a scalar field m^{-1} ∇ .divergence of a vector field m^{-1} Θ_D diffraction angle- σ^M Maxwell stress vectorN/m² δ_p penetration depthm α fill ratio-	ϵ_t	complex permittivity	F/m
σ conductivity S/m^2 ∇ gradient of a scalar field m^{-1} ∇ .divergence of a vector field m^{-1} Θ_D diffraction angle- σ^M Maxwell stress vector N/m^2 δ_p penetration depthm $lpha$ fill ratio-	ρ	mass density	kg/m ³
∇ gradient of a scalar field m^{-1} ∇ .divergence of a vector field m^{-1} Θ_D diffraction angle- σ^M Maxwell stress vector N/m^2 δ_p penetration depthm α fill ratio-	ϕ	electrical scalar potential	V
∇ .divergence of a vector field m^{-1} Θ_D diffraction angle- σ^M Maxwell stress vector N/m^2 δ_p penetration depthmæfill ratio-	σ	conductivity	S/m^2
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σ^M Maxwell stress vectorN/m² δ_p penetration depthmæfill ratio-	abla.	divergence of a vector field	m^{-1}
δ_p penetration depth m æ fill ratio -	Θ_D	diffraction angle	-
æ fill ratio -	σ^M	Maxwell stress vector	N/m^2
	δ_p	penetration depth	m
δ_c skin depth m	æ	fill ratio	-
	δ_c	skin depth	m

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1. TIKKA-A., AL-SARAWI-S., AND ABBOTT-D. (2009). Loading analysis of a remotely interrogatable passive microvalve, *Recent Advances in Sensing Technology - Lecture notes in Electrical Engineering Series*, Springer-Verlag, Accepted for Publication.

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2. TIKKA-A., AL-SARAWI-S., AND ABBOTT-D. (2008). Modelling a surface acoustic wave based remotely actuated microvalve, *Smart Materials & Structures*, 18, p. 045014.

3. TIKKA-A., AL-SARAWI-S., AND ABBOTT-D. (2008). Acoustic wave parameter extraction with application to delay line modelling using finite element analysis, *Sensors and Transducer Journal*, 95(8), pp. 26-39.

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4. TIKKA-A., AL-SARAWI-S., AND ABBOTT-D. (2009). Contactless energy transfer for a SAW based implanted microvalve, *Proc. of IEEE Regional Symposium on Micro and Nano Electronics*, pp. 513-517.

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